GENERATOR SELECTION

Generators must be sized to handle their load based on the <u>continuous</u> KW, kilowatt load, and KVA, kilovoltamp load, and the worst case <u>starting load</u> KW + KVA. They must be derated for temperature and elevation. They are sized also on whether they are continuous or standby use. The following steps are used to obtain information:

- 1. Select System Voltage and Phase
 - a. <u>Three phase</u> 120/208V, 3 phase, 4W wye; 277/408, 3 phase, 4W wye; * 120/240V 3 phase, 4W Delta

* Should not use on generator as it overloads 1 phase if there are large 120 volt loads.

- b. <u>120/208V, 3 phase, 4W</u>- This is a good choice for a three phase system because you can balance 120 volt loads around the wye to equally load the generator. 208V single phase and 208V three phase loads can be used as well as 120V single phase loads. Motors must be rated 200 volt operation; 240 volt resistance heating equipment used on a 208V generator will only produce 75% of its rated KW output.
- c. <u>277/480, 3 phase, 4W</u>- This voltage is usually used on large systems to reduce incoming service size, wire size and distribution equipment size. Fluorescent and other discharge lighting can be used at 277 volts. 480 volt single phase, 480V three phase, and 277 volt single phase loads can be used on this system. Also good for minimizing voltage drops on long runs. Disadvantages are that a step down transformer is required to get 120/208 or 120/240 volt power for lights and outlets. Motors should be started directly from the generator buss, <u>not</u> from a step down transformer to minimize voltage drop.
- d. <u>120/240V, 3 phase, 4 W Delta</u>- This is the least desirable voltage to use if there is a large amount of 120 volt load. The generator can not be balanced and may overheat the windings. Advantages are 240 volt motors and equipment are more common than 200 volts.
- e. <u>120/240V, 1 phase, 3W</u> This is the standard voltage for single phase systems. Motors are limited to 10HP maximum. Either 120 volts or 240 volts can be used to supply loads. 120 volt loads must be balanced across the generator L1 to N and L2 to N. Disadvantages are that single phase motors are more unreliable than three phase motors, especially capacitor start motors. The voltage drop is higher in single phase systems for a given load for the same wire size used in 3 phase systems.

- 2. <u>List Loads</u> (for each load, list the following)
 - a. Voltage
 - b. Phase
 - c. Horsepower if motor, STARTING CODE LETTER
 - d. Running KW, Running KW= starting KW if PF = 1
 - e. Starting KW
 - f. Running KVA, Running Power Factor
 - g. Starting KVA, Starting Power Starting
 - h. Motor full load amps from nameplate

See Table 2 Onan book for motor data

3. <u>Resistive Loads</u>

Resistive loads consist of incandescent lights, water heaters, electric heaters, stoves, and electric furnaces. Power factor = 1, KW = KVA. Running and starting KW are the same.

4. Motors and Inductive Loads

Motors are inductive loads with KVA always larger than KW. The power factor running usually is between 0.6 and 0.85.

$$P.F. = \frac{KW}{KVA}$$
$$KW = (KVA) (PF)$$
$$KVA = \frac{KW}{PF}$$

2

Determine locked rotor code letter from Table 2, A-R, for a given horsepower motor. If the motor is existing, use nameplate data. If this is a new installation, use shaded blocks in Table 2. Find starting KVA from Table 3. Find starting power factor from Table 2. Calculate KW starting = (KVA start) (PF start).

To find starting KVA if only locked rotor amps are known;

$$\frac{1 \text{ phase}}{\text{KVA start}} = (\text{locked rotor amps}) (\text{voltage})$$

$$\frac{5 \text{ phase}}{\text{KVA start}} = \sqrt{3} (\text{locked rotor amps}) (\text{voltage})$$

For submersible water pumps only, use page 24-17,18 for motor data.

To find running KW and KVA if only full load current is known;

<u>1 phase</u> KVA	=	(I full load current) (voltage)								
Kwrun	=	(KVArun) (power factor running)								
See Table 2 for given HP, $PF = \frac{KW}{KVA}$										

5. Voltage Dip

Determine maximum percentage voltage dip. This is basically what sizes the generator. If voltage dip is too large, the motor will over heat or not start because there is not enough torque to accelerate the motor. Motor torque falls off approximately as the product of reduced squared. For example, with a 30% voltage dip resultant torque, it will be:

T = (.70 volts) 2 = .49 or 49% available torque.

Voltage dip is usually expressed as a percent dip of nominal voltage as measured by light beam oscillograph or pen recorder on the first cycle. This is the voltage dip due to the generator winding resistance before the regulator tries to make the voltage recover. This will last anywhere from 1 cycle to 30 cycles depending on the response of the generator. This voltage dip is usually called the initial or transient voltage dip. After the regulator makes the generator recover, there is a recovery voltage dip from 5 cycles until the motor reaches 70%-90% of synchronous speed.

The sustained voltage dip must be kept low enough to insure that relays and motor starter do not drop out.

6. Voltage Dropout Problems on Motor Control Systems

Recovery dip should be limited to 5% if there are control relays and motor starters unless special precautions are taken in the control system power supply. If the voltage dips low enough to drop out the starters, the motor starters will chatter, burning out the motor. There are three ways to prevent system oscillation.

- a. Size generator for 5% initial voltage dip (RMS). This will result in a larger generator size.
- b. On small systems where the generator is the only power source, utilize D.C. voltage from the generator battery as the control power.
- c. If the generator is a standby unit, utilize a constant voltage transformer in the control system power supply, such as a Sola CVS. This will keep the voltage to the control relays to within 95% of nominal voltage with up to 30% dip on the primary.

7. <u>Recovery Voltage Dip</u>

This voltage dip occurs from 5-30 cycles after load is applied. This dip should be no more than 5%. This dip is not given in the manufacturers standard literature. Each application must be checked with the generator manufacturer.

8. Total Voltage Dip

The total voltage dip is the sum of the generator voltage dip and the voltage drop to the load on the conductors. This total should not exceed 10% on starting.

9. <u>Resistive Voltage Dip</u>

For resistive loads, the starting and running voltage dip in the conductors is the same. The formula for voltage drop is:

 $\frac{1 \text{ phase Voltage Drop}}{Vd= 2(I) (Z) (L)}$

I = Current Amps

Z = Total impedance - ohms per 1,000 feet of conductor

L = One way length of conductors - kilo feet

P.F. = Power Factor = 1.0 (use this when looking up Z)

Refer to Electrical Design/Operation Maintenance Manual R6-1980 (pages 8-1, 8-6 for voltage drop tables). Size feeders for resistive loads at 2% voltage drop.

3 phase Voltage Drop
 $Vd = (\sqrt{3}) (I) (Z) (L)$ P.F. = 1.0% Vd = Vd (100)
Base volts2 volts (100)
240 volts= .8%

Use same tables for 1 phase, or 3 phase voltage drop.

Reactive Dip Example

Loads Voltage: 120/240V, 1 phase Resistive load: 2 KW, 240V; 1 KW, 120V; 1.5 KW, 120 volt. Total resistive load:

$$I = \frac{2 \text{ KW}}{.23 \text{ KV}} = 8.7 \text{ A on } \text{L1, and } \text{L2}$$

$$I = \frac{1 \text{ KW}}{.115 \text{ KV}} = 8.7 \text{ A on } \text{L1}$$

$$I = \frac{1.5 \text{ KW}}{.115 \text{ KV}} = 13.04 \text{ on } \text{L2}$$

Total Resistance Load:

	L1	L2
2 KW	8.7A	8.7A
1 KW	8.7A	0
1.5 KW		13.04
	17.4	21.74

Use the 21 amps for sizing the generator. A voltage drop calculation normally does not need to be done if the generator is close to the distribution panel where the loads receive their power, say 25 feet or less. Conductors for loads must be sized for their ampacity, use NEC 310-16 first, then check for voltage drop.

For the 2KW load, 2 #12 Cu wire would be used with a 2 pole 15 amp breaker.

For the 1 and 1.5 KW loads 2 #12 Cu with a 1 pole 20 amp breaker would be used.

Refer to O&M Manual, Section 3 for sizing conductors.

These are the wire sizes for ampacity. Now check voltage drop. NEC ampacity tables do not take into account voltage drop.

Conductor Voltage Drop for Resistive Loads and Wire Sizes

I = 8.7A Length = 250 feet #12 CU in conduit PF = 1 Vd = 2 I Z L from page 24-14 #12, Z = 1.62 / Kft. Vd= (2) (8.7A) (1.62 /Kft.) (.25Kft.) = 7.04 volts %Vd = $\frac{Vd 100}{Base volts} = \frac{(7.04V)(100)}{230V} = 1.92\%$

So #10 is o.k. for voltage drop.

Motor Voltage Drop In Feeder Conductors

Motor 2HP, 230V, 1 Phase, code letter J, capacitor start, conductor length = 300 ft. Full load current from NEC table 430-148, I = 12 amp.

Onan Book, Table 2, 2 HP, Code J

Starting KVA = 16.4 KVA

Run KVA = 2.6 KVA

Start KW = (KVA start) (PF start) = (16.4) (.9) = 14.76 KW

Run KW = 1.8 KW

Istart = $\frac{16.4 \text{ KVA}}{.23 \text{ KV}}$ = 71.30 amp

Irun= 12 amp

Inrush = $\frac{71.30 \text{ amp start}}{12 \text{ amp run}}$ = 5.9 times running current

So if we size the wire for 1% voltage drop on running, we will have about a 6% voltage drop on starting. If this 6% voltage drop is added to the generator recovery voltage drop of 5%, the total overall voltage drop will be about 11%. NEMA says motors need 90% of voltage to start.

Size Conductors

Vd = 2 I Z L $Z = \frac{Vd}{2 I L} \qquad L = .3Kft.$ Vd = 1% = (.01) (230V) = 2.3V $Z = \frac{2.3}{2(12 \text{ amp}) (.3 Kft.)} = .319/Kft.$ (@.8 P.F. running, page 8-4 O&M, CU wire #4, Z = .2365/Kft. Voltage Drop for #4 CU Vd = 2 I Z L = (2) (12) (.2365) (.3 Kft.) = 1.70V

% Vd = (1.70V)(100) = .74%230V Starting voltage drop (cable only) = (.74%)(5.9) = 4.14%

Sizing Gnerator

WHEW—We're finally at the good stuff. How do you size the generator itself? Well first of all, <u>don't</u> use the tables in the Onan book I just gave you. They do not cover voltage drop. Each case must be referred to the manufacturer to size the generator. If the generators are loaded to their maximum output indicated in the tables, there may be as much as 10% or more voltage dip without considering wire voltage drop which may not work with a system with motors. Anyway, on with the procedure:

1. Given Loads

2HP, 230V, 1 phase, code J Start KVA = 16.4 Run KVA = 2.6 Start KW = 114.76 start P.F. = 0.8Run KW = 1.8

Resistance Loads – 4.5 KW, 230V, 1 phase Assume resistance loads are balanced

- 2. Go to Onan Load Sheet, page <u>24-9</u>; write down resistive loads on column 12 and 13, KW = KVA so entries are the same on line 1.
- 3. List motor loads with the worst case (largest load applied last) in order on the load form, line 2-16.

If a system manual motor start, starting largest motor first may reduce generator size. If other loads are already running and this starting sequence is not followed, the generator may be overloaded or motors may drop out or not start.

List the following items from Table 2, Onan Book, page 7 for each motor load:

HP Starting Code Letter Volts Starting KVA, starting power factor Starting KW Running KVA Running KW

 Column 10: Add column 6 to previous line column 12. Column 11: Add column 7 to previous line column 13. Column 12: Add column 8 to previous line column 12. Column 13: Add column 9 to previous line column 13. 5. Look at the largest numbers in columns 10, 11, 12 and 13. Generator output must be greater than these numbers.

<u>WARNING</u> – THIS DOES NOT TAKE INTO ACCOUNT VOLTAGE DROP ON GENERATOR. CONSULT MANUFACTURER AT THIS POINT.

Look at Example pages 24-9.

	10	11	12	13
	Max. KVA	Max. KW	Cont. KVA	Cont. KW
	20.9	19.2	7.1	6.3
Onan generator 20ES	42	22	25	20

This applies to Onan only, other generators by other manufacturers have different characteristics.

In this case, a 20 KW generator would handle the continuous KVA and KW, and maximum KVA and KW. Refer to pages 3-6, Onan T-009 Generator Selection Guide.

Sizing for Submersible Water Pump Motors

Submersible water pump motors have a higher than normal locked rotor code letter and running current than Onan tables shown for average motors. The running current is higher than NEC 430-148 when run at their service factor amps. Use the following attached tables:

CL	STOM	ER									_	RECOMMI	ENDED U	NIT		
AC	DRES	is														PHASE
CI	TY				ST	ATE			ZIP _			KW		KVA .		PF
DE	ALER	R/DISTI	RIBU	TOR							-					Temperature
SA	LESM	AN						ė	<u> </u>		_					KVA
ON	AN R	EPRES	ENT	ATIVE	<u> </u>						- 21	MAXIMUM	VOLTAG	E DIP		
		R INFO Fro Dr nam	M			DUCED LTAGE DTOR ARTING	STA	OTOR RTIN OAD	G	RUN		LOAD INCO STAR	PLUS OF MING TING		ILATED Ad	NOTES: NAME OF LOAD, Voltage dip, etc.
	I	2	3	4		5	6		7	. 8	9	10		2 Cont. KVA	13	
	HP	Code	φ	Volts	Тар	Mult.	KVAs		K₩s	KVA				Cont. KVA Add 8to 12		
1							1	<u>۱</u>						4.5	4.5	RESISTANCE LOAD
2	3	Т	1	230			16.4	.8	14.76	2.6	1.8	20.9	192	7.	6.3	Motor
3			Pr			OES	Ger	1	Øco	nnec	+	212	, 22	25	20	
4														ON		
5																meon
6						Iγ	time	S	7/48	TL	ARC	BEST	MOTO	R LA.	STT	OGIVE
7						CA	SE	57	AR	TIN	6	LOAD	1 .			
8				64	ene	evat	B L F	ηι	5-1	В	-e .	capa	ole	ofo	rouid	Îng.
9				Ma	2×1	mum	KV	A	an	θK	w	and	PL.	50 B 2	ELAR	GER
10												ALK				
11				•						-	-	2				
12				TH	E	20E	5 Pu	pau	re	Ge	n.	is La	mar e	aough	400	continuous
13							KV/							L, KY		, <u> </u>
14									ecl	- w	ith	g-en-	erato	1 mai	nu fac	turer
15					40	vo	L tad	e	24	00	an	0 4	or M	AXK	wall	owable.
16																

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							<u> </u>									PHASE
							· · · · · ·				w.,					PF
	•	.					-					DERATIN	GS: Altitu		e	
DE/	ALER	/DIST F	RIBU	TOR					-	~`.	_	Fuel				Temperature
5AL	.ESM/	AN						į.	v		_			· ·		KVA
אט	AN R	EPRES	ENT	ATIVE			·····		•		- .	MAXIMUM	VOLTAG	E DIP		·
	мото	R INFO Fro Dr Nam	RMA	TION	REI VOL MC	DUCED TAGE DTOR ARTING	MC ST A	OTOR RTIN OAD	G	MO' RUN	TOR NING DAD	LOAD LOAD INCO	MING	ACCUMULATED LOAD		NOTES: NAME OF LOAD, Voltage dip, etc.
	1	2	3	4		5 ·	6		7	8	9	10				
	HP	Code	ø		Тар	Mult.	KVAs	PF	KWs	KVA	KW		1	Cont. KVA Add 8 to 12		
	nr	Code	<u> </u>	10103									Hod Y de lo			
4					<u> </u>				1. 12							
2											,		*			· · · · · · · · · · · · · · · · · · ·
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14					<u> </u>											
15					 										··· ··· ···	
12				·	_				L	L	 			↓		

Voltage Drop Equations

Voltage Drop Equations

Voltage Drop = $\sqrt{3}$ I (R Cos θ + X Sin θ) L 3Ø

Voltage Drop = 21 (R $\cos \theta + \sin \theta$) L 1Ø

Voltage Drop = in volts (V)I = Current in Amperes (A)R = Conductor Resistance in ohms/1000 ft.X = Conductor inductive reactance in ohms/ 1000 ft.L = One way length of circuit (source to load) in thousands of feet (K ft.) Z = Complex impedance ohms/ 1000 ft. Obtain from Tables. θ = Phase angle of load.

 $\cos \theta$ = Power Factor: Motors see 6-5,6-6, .6-.8 is usual see 5-1 to 5-8 for power factor calculations, also 8-2

Given Voltage Drop, Find wire size:

Voltage Drop $3\emptyset = \sqrt{3} I(Z) L$

Z = Voltage Drop= <u>Vd</u> √3 I L $\sqrt{3}$ IL

Voltage Drop $1\emptyset = 2 I (Z) L$

 $Z = \frac{\text{Voltage Drop}}{\sqrt{2 \text{ I L}}} = \frac{\text{Vd}}{\sqrt{2 \text{ IL}}}$

Procedure (Example)

- 1. Assume a voltage drop, say 2%, Base voltage 230V, $1\emptyset$ Vd = .02(230V) = 4.8volts drop. Direct burial Copper.
- 2. Current and Distance must be known I = 30A, L = .56K Ft. = .56K Ft. Power Factor must be known, PF = .85
- 3. Solve for Z: Z = Vd/2IL = 4.8V/2 (30A) (.5K Ft.) = .16 Ω / K Ft.

4. Look up Z in tables at .16 Ω / K Ft, 85 P.F. Copper Direct burial in nonmagnetic conduit. #1 CU, Z = .16 Ω / K Ft \therefore smaller impedance so use #1 Always use wire with the next smaller impedance Z per 1,000 feet than that calculated.

Three Phase Voltage Drop

Example:

Three phase, Direct Burial Copper

- 1. Vd = $\sqrt{3}$ (I) (Z) (L)
- 2. Given: Voltage 230 V, 3 phase, load 5 KW P.F. = 1 heater, L = 480 ft., find wire size.
- 3. Assume a voltage drop, say 2%, base voltage, 230 volts. Voltage drop maximum = (.02) (230 volts) = 4.6 Volts. I = $\frac{5 \text{ KW}}{23 \sqrt{3}}$ = 21.7A

Solve for Z:

 $Z = \frac{\text{Voltage Drop}}{\sqrt{3} \text{ IL}} = \frac{4.6 \text{ Volts}}{\sqrt{3} (21.7 \text{ A}) (.48 \text{ K FT})} = .0254 \text{ ohms/K FT}.$

Look Z up in Table on voltage drop charts. @ P.F. = 1.0 Copper Direct Burial Table 75 degrees C. Use next smaller Z for wire size. Nonmagnetic conduit. 500 MCM = .0270 Ω / KFT, 600 MCM = .023 Ω / KFT Use 600 MCM because its impedance is less than that calculated.

Power Factor

 $PF = \cos \theta = \frac{KW}{KVA}$

Given 10 KW, 12 KVA Load, find PF: PF = 10KW = .83 12 KVA

CONDUCTOR IMPEDANCES

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POWER FACTOR

1.00.95 .90 .85 .80 .75 .70 .65 .60 .55 .50 .45 .40 .35

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	14	3.062	2.932	2.788	2.642	2.494	2.346	2.197	2.047	1.897	1.747	1.596	1.445	1.293	1.142	
	12	1.932	1.858	1.771	1.681	1.590	1.498	1.406	1.313	1.219	1.125	1.031	0.936	0.841	0.746	
	10	1.214	1.176	1.125	1.071	1.016	0.960	0.903	0.846	0.788	0.730	0.672	0.613	0.554	0.495	ס
Γ	ш 8	0.811	0.793	0.762	0.729	0.694	0.658	0.621	0.584	0.546	0.509	0.470	0.432	0.393	0.354	PE
	<u>N</u> 6	0.510	0.505	0.488	0.469	0.449	0.427	0.405	0.383	0.360	0.337	0.314	0.290	0.266	0.242	7
	<mark>ଡ</mark> ଼ 4	0.321	0.324	0.316	0,306	0.294	0.282	0.269	0,256	0.243	0.229	0.215	0.200	0.186	0.171	1_
	ш 3 і							1 a								Z
	<u> </u>	0.202	0.210	0.207	0.202	0.196	0.190	0.183	0.175	0.168	0.159	0.151	0.143	0.134	0.125	Ň
	≥ 1	0.160	0.169	0.168	0.166	0.162	0.157*	0.152	0.147	0.141	0.135	0.129	0.122	0.116	0.109	AG
-	1/0	0.128	0.138	0.138	0.137	0.134	0.131	0.128	0.124	0.120	0.115	0.110	0.105	0.100	0.095	Z
	2/0	0.102	0.113	0.115 -	0.114	0.113	0.111	0.109	0.106	0.103	0.100	0.097	0.093	0.089	0.085	E
	3/0	0.080	0.092	0.095	0.095	0.095	0.094	0.093	0.091	0.089	0.087	0.085	0.082	0.079	0.076	- - -
	4/0	0.064	0.076	0.079	0.080	0.081	0.080	0.080	0.079	0.078	0.076	0.075	0.073	0.071	0.068	
7	250	0.055	0.067	0.071	0.072	0.073	0.074	0.073	0.073	0.072	0.071	0.070	0.069	0.067	0.065	CO
	300	0.046	0.059	0.063	0.065	0.066	0.067	0.067	0.067	0.067	0.066	0.065	0.064	0.063	0.062	Z
	350	0.037	0.051	0.055	0.057	0.059	0.060	0.061	0.061	0.061	0.061	0.061	0.060	0.060	0.059	סנ
	400	0.035	0.049	0.053	0.056	0.057	0.059	0.059	0.060	0.060	0.060	0.060	0.059	0.059	0.058	UIT
	500	0.029	0.042	0.046	0.049	0.051	0.052	0.053	0.054	0.054	0.055	0.055	0.054	0.054	0.053	
	600	0.025	0.038	0.043	0.046	0.048	0.049	0.051	0.051	0.052	0.052	0.052	0.052	0.052	0.052	7
	700															5
	750	0.021	0.034	0.038	0.041	0.043	0.045	0.046	0.047	0.048	0.049	0.049	0.049	0.049	0.049	ဂ

6/17/02

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CONDUCTOR _ IMPEDANCES

POWER FACTOR

1.00.95.90.85.80.75.70.65.60.55.50.45.40.35

			· · · ·	_												
1	14	3.062	2.927	2.782	2.634	2.485	2.336	2.186	2.036	1.885	1.734	1.583	1.431	1.280	1.128	
-	12 -	1.932	1.854	1.765	1.673	1.581	1.488	1.395	1.301	1,207	1.1,12	1.018	0.923	0.828	0.732	ĺ
	10	1.214	1.172	1.118	1.063	1.007	0.950	0.892	0.834	0.776	0.718	0.659	0.600	0.540	0,481	
ш	8	0.811	0.789	0.756	0.721	0.684	0.648	0.610	0.572	0.534	0.496	0.457	0.418	0.379	0.340	
IZI	6	0.510	0.501	0.482	0.462	0.440	0.418	0.396	0.373	0.349	0.326	0.302	0.278	0.254	0.229	
S	4	0.321	0.320	0.310	0.299	0.287	0.274	0.260	0.247	0.233	0.218	0.204	0.189	0.174	0.159	0
ш	3						- - 1	* .e						. •		Ū
IR	2	0.202	0.206	0.202	0.196	0.189	0.182	0.174	0.166	0.158	0.150	0.141	0.132	0.123	0.114	모
3	1	0.160	0.166	0,163.	0.160	0.155	0.150	0.144	0.138	0.132	0.126	0.119	0.112	0.105	0.098	RE
1	/0	0.127	0.134	0.133	0.130	0.127	0.123	0.119	0.115	0.110	0.105	0.100	0.095	0.090	0.084	Ö
2	/0	0.101	0.109	0.109	0.108	0.106	0.103	0.101	0.098	0.094	0.091	0.087	0.083	0.079	0.075	1
3	/0	0.076	0.085	0.087	0.086	0.086	0.084	0.083	0.081	0.079	0.076	0.074	0.071	0.068	0.065	B
4	/0	0.063	0.072	0.074 -	0.074	0.074	0.073	0.072	0.071	0.069	0.068	0.066	0.064	0.061	0.059	UR
2	50	0.054	0.063	0.065	0.066	0.067	0.066	0.066	0,065	0.064	0.062	0,061	0.059	0.057	0.056	A
3	00	0.045	0.055	0.057	0.059	0.059	0.059	0.059	0.059	0.058	0.057	0.056	0.055	0.054	0.052	
3	50	0.036	0.047	0.050	0.051	0.053	0.053	0.053	0.053	0.053	0.053	0.052	0.051	0.050	0.049	ĺ
4	00	0.034	0.044	0.047	0.049	0.050	0.051	0.051	0.052	0.051	0.051	0.051	0.050	0.049	0.048	
5	00	0.027	0.037	0.041	0.043	0.044	0.045	0.045	0.046	0.046	0.046	0.046	0.045	0.045	0-044	
6	00	0.023	0.034	0.037	0.039	0.041	0.042	0.043	0.043	0.043	0.044	0.043	0.043	0.043	0.043	
7	00	· .														7
7	50	0.019	0.029	0.032	0.035	0.036	0.038	0.039	0.039	0.040	0.040	0.040	0.040	0.040	0.040	U
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4	14	5.054	4.817	4.571	4.323	4.075	3.825	3.575	3.325	3.074	2.823	2.572	2.321	2.070	1.818	1
•	12	3.186	3.043	2.890	2.736	2.580	2.424	2.268	2.111	1.954	1.796	1.638	1.481	1.322	1.164	N
	10	2.000	1.916	1.823	1.727	1.631	1.535	1.437	1.340	1.242	1.144	1.045	0.947	0.848	0.749	5
ш	8	1.258	1.211	1.155	1.097	1.038	0.978	0.918	0.857	0.797	0.736	0.674	0.613	0.551	0.489	NIN
N	6	0.847	0.821	0.785	0.747	0.709	0.670	0.630	0.590	0,550	0.510	0.469	0.428	0.387	0.346	Ī
ပ	4	0.532	0.521	0.500	0.478	0.455	0.432	0.408	0.383	0.359	0.334	0.309	0.284	0.258	0.233	S
ш	3															
I.R.	2	0.335	0.332	0.321	0.308	0.295	0.281	0.267	0.252	0.237	0.222	0.207	0.191	0.176	0.160	Z
≥	1	0.265	0.266	0.259	0.250	0.240	0.230	0.219	0.208	0.197	0.185	0.174	0.162	0.149	0.137	Z
1	/0	0.210	0.212	0.207	0.201	0.193	0.185	0.177	0.169	0.160	0.151	0.142	0.132	0.123	0.113	A
2	/0	0.167	0.171	0,168	0.163	0.158	0.152	0,146	0.139	0.133	0.126	0.119	0.111	0.104	0.096	GN
3	/0	0.133	0.138	0.137	0.134	0.130	0.126	0.121	0.116	0.111	0.106	ó.101	Q,Q95	0.089	0.084	Ш
4	/0	0.106	0.112	0.112	0.110	0.108	0.105	0.102	0.098	0.094	0.090	0.086	0.082	0.078	0.073	
2	50	0.089	0.097	0.097	0.096	0.094	0.092	0.090	0.087	0.084	0.081	0.078	0.074	0.071	0.067	ဂ
3	00	0.075	0.082	0.083	0.083	0.082	0.081	0.079	0.077	0.075	0.072	0.069	0.067	0.064	0.061	C
	50	0.064	0.072	0.074	0.074	0.073	0.072	0.071	0.069	0.068	0.066	0.064	0.061	0.059	0.057	0 Z
4	00	0.056	0.065	0.066	0.067	0.067	0.066	0.065	0.064	0.063	0.061	0.059	0.058	0.056	0.053	
5	00	0.045	0.054	0.056	0.057	0.058	0.057	0.057	0 ⁻ .056	0.055	0.054	0.053	0.052	0.050	0.049	L I
6	00	0.038	0.048	0.050	0.051	0.052	0.052	0.052	0.052	0.052	0.051	0.050	0.049	0.048	0.047	
7	00	0.033	0.043	0.045	0.047	0.048	0.048	0.048	0.048	0.048	0.047	0.047	0.046	0.045	0.044	00
7	50	0.031	0.040	0.043	0.044	0.045	0.046	0.046	0.046	0.046	0.045	0.045	0.044	0.043	0.043	õ

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	14	5.054	4.814	4.566	4.318	4.068	3.818	3.567	3.317	3.066	2.814	2.563	2.311	2.060	1.808	
	12 -	3.186	3.039	2.885	2.730	2.574	2.417	2.260	2.102	1.945	1.787	1.629	1.471	1.312	1.154	
	10	2.000	1.913	1.818	1.722	1.625	1.527	1.429	1.331	1.233	1.135	1.036	0.937	0.838	0.739	
Ш	8	1.258	1.208	1.150	1.091	1.031	0.971	0.910	0.849	0.788	0.726	0.665	0.603	0.541	0.479	
N	6	0.847	0.817	0.780	0.742	0.702	0.663	0.622	0.582	0.541	0.500	0.459	0.418	0.377	0.335	OR
S	4	0.532	0.517	0.496	0.473	0.449	0.425	0.400	0.376	0.351	0.326	0.300	0.275	0.249	0.223	
Ш	3						u € 2 1							. •		DIR
E	2	0.335	0.329	0.317	0.304	0.290	0.275	0.260	0.245	0.230	0.215	0.199	0.183	0.167	0.151	Ĩ
>	1	0.265	0.262	0.253	0.243	0.233	0.221	0.210	0.198	0.187	0.174	0.162	0.150	0.138	0.125	CT
1	/0	0.210	0.210	0.203	0.196	0.188	0.179	0.171	0.162	0.153	0.143	0.134	0.124	0.115	0.105	-
2	/0	0.167	0.16 8	0.164	0.159	0.153	0.147	0.140	0.133	0.126	0.119	0.112	0.104	0.097	0.089	BU
З	/0	0.133	0.137	0.135	0.132	0.128	0.124	0.119	0.114	0.109	0.104	0.098	0.092	0.087	0.081	R
4	/0	0.105	0.109	0.108	0.105	0.102	0.099	0.095	0.091	0.087	0.083	0.079	0.074	0.070	0.065	AL
2	50	0.089	0.094	0.093	0.092	0.089	0.087	0.084	0.081	0.078	0.074	0.071	0.067	0.063	0.060	
З	00	0.074	0.080	0.080	0.079	0.077	0.075	0.073	0.071	0.068	0.066	0.063	0.060	0.057	0.054	
З	50	0.064	0.068	0.068	0.067	.0.065	0.064	0.062	0.060	0.058	0.055	0.053	0.050	0.048	0.045	
4	00	0.056	0.062	0.063	0.063	0.062	0.061	0.060	0.058	0.057	0.055	0.053	0.051	0.049	0.046	
5	5Q0	0.045	0.051	0.053	0.053	0.053	0.052	0.051	0.051	0.049	0.048	0.047	0.045	0.044	0.042	
6	00	0.038	0.045	0.046	0.047	0.047	0.047	0.047	0.046	0.045	0.044	0.043	0.042	0.041	0.040	
7	00	0.033	0.040	0.041	0.042	0.043	0.043	0.043	0.042	0.042	0.041	0.040	0.039	0.038	0.037	
7	50	0.030	0.037	0.039	0.040	0.041	0.041	0.041	0.040	0.040	0.039	0.039	0.038	0.037	0.036	00

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Submersible Motors Engineering Manual 4-inch Three Wire Submersible Water Well Motors 60 Hertz Representative Loading and Performance Data

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575 3 1.15 332994 6.1 5000 7.0 5800 900 20 8 K 42 7-1/2 200 3 1.15 334066 27.0 7700 30.8 9000 900 80 35 J 158 230 3 1.15 333625 23.5 7700 26.8 9000 900 70 30 J 143 460 3 1.15 333005 11.7 7700 13.4 9000 900 35 15 J 72 575 3 1.15 333732 9.3 7700 10.7 9000 900 30 12 J 57													K	52
7-1/2 200 3 1.15 334066 27.0 7700 30.8 9000 900 80 35 J 158 230 3 1.15 333625 23.5 7700 26.8 9000 900 70 30 J 143 460 3 1.15 333005 11.7 7700 13.4 9000 900 35 15 J 72 575 3 1.15 333732 9.3 7700 10.7 9000 900 30 12 J 57			२											42
230 3 1.15 333625 23.5 7700 26.8 9000 900 70 30 J 143 460 3 1.15 333005 11.7 7700 13.4 9000 900 35 15 J 72 575 3 1.15 333732 9.3 7700 10.7 9000 900 30 12 J 57	7-1/2		ž						the second s	and the second data second data and the second data and the second data and the second data and the second data		35		158
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575 3 1.15 333732 9.3 7700 10.7 9000 900 30 12 J 57			3							900			J	72
						1				900	30	12		<u> </u>
	10	460	3	1.15	332992	15.6	10100	17.6	11700	900	45	20		108
575 3 1.15 333734 12.5 10100 14.1 11700 900 40 20 K 86									11700	900	40	20	K	86

Submersible Motors Engineering Manual 6-Inch Submersible Water Well Motors 60 Hertz Representative Loading and Performance Data

					•				·	Max.	Circ. Brk.	Dual		•
			<i>a</i> .			4	ردی ک ^{رد} اور از مراجع افغانی میلا		imum Taradaa	Thrust	or Std.	Ele-	1/17	Locked
Rated			Service	Winding	Rated	нР		Input(S		Load Pounds	Fuse	ment	Code	Rotor
HP		PH.		Number	Amps		Watts.	Amps	Watts 5820	1500	80 80	35	i se	99 99
2	230	<u> </u>	1.15	332497	26.0	47		<u>29.5</u> 40.0	8500	1500	100	45	<u> </u>	145
7-1/2	230	1	1.15	332529	34.5		7300		11500	3500	150		F	223
10	230	1	1.15	334978	45.0	<u>.</u>	4800	52.0	5600	1500	50	25	Ĵ	103
5	200	3	1.15	333394	17.0 14.8		4800	19.1 16.6	5600	1500	45	20	J	90
	230	3	1.15	332517			4800	8.3	5600	1500	25	10	J	45
	460	3	1.15	334680	7.2		4800		5600		20	8	J	36
- 1/0	575	3	1.15	332679	5.9			6.6	8200	<u>1500</u> 1500	70	30	J	156
7-1/2	200	3	1.15	333395	24.2		7000	27.5	8200	-		30	J	136
	230	3	1.15	332493	21.0		7000	23.9	8200	1500	70	30 15	J	68
	460	3	1.15	334681	10.5		7000	11.9	-	1500 1500	25	12	J	54
	575	3	1.15	332649	8.4		7000 9600	<u>9.5.</u> 36.8	11100	3500	100	40	K	235
10	200	3	1.15	333396	32.1		9600 9600		~11100	3500	80	35	K	204
	230	3	1.15	332475 334682	27.9		9600 -	1 7	11100	3500	40	20	K	102
	460	3	1.15		13.9		9600 -	12.8	11100	3500	35	15	K	82
· · · · · ·	575	3	1,15	332650	47.2	·		53.6	16100	3500	150	60	J	306
] -	200	3	1.15	333359	41.0		13900	46.6	16100	3500	125	60	J	266
15	230	3	1.15	332528			13900	23.3	16100	3500	60	30	J	133
	460	3	1.15		20.5		13900	18.6	16100	3500	+ 50	25	J	106
	575	3	1.15	332760			13900	70.2	21600	3500	200	- 20	J	430
20	200	3	1,15	333397	60.3		18300 18300	61.0	21600	3500	175	70	J	374
	230	3	1,15	333230	52.4			1	21600	3500	80	. 35	J	187
	460	3	1.15	334684	26.2		18300	30.5	21600	3500	70	30	J	150
05	575	3	1.15,	332790	21.0		18300 22600	86.3	26100	3500	225	100	K	598
25	200	3	1.15	333398	74.8		22600	75.0	26100	3500	200	90	ĸ	520
	230	3	1.15	333595	65.0		22600	37.5	26100	3500	100	45	K	260
	460	3	1.15	334685	32.5		22600		26100	3500	80	35	K	208
- 20	575	<u></u>	1.15	333338	26.0	<u> </u>	27000	30.0	31500	3500	300	125	J	662
30	200	3	1.15	333399	92.0		•			3500	250	110	J	576
	230	3	1.15	333310	80.0		27000 27000	92.0 46.0	31500 31500	3500	125	50	J	288
	460	.3	1.15	334686	40.0		•	₹ 36.8	31500	3500	100	· 40	J	230
	575	3	1.15	333416	32.0		27000 36000	60.0	42000	3500	150	70	J	400
40	460	3	1.15	333183	51.5			48.0	42000 42000	3500	125	60	J	320
	575	<u></u>	1.15	333108	41.0	····	<u>36000</u> 44000	75.0	<u>42000</u> 52000	3500	200	90	K	520
50	460	3	1.15	333594	1.		44000	60.0	52000	3500	150	90 70	K	416
· .	575	3	1.15	333500	53.5		<u>++</u> 000	1.00.0	J2000	1 2200	1-20		<u> </u>	-710

Table 430-1	50. Full-Load Cu Alternating-Current	rent*
Three-Phase	Alternating-Current	Motors

	Induction Type Squirrel-Cage and Wound-Rotor Amperes					Synchronous Type †Unity Power Factor Amperes			
HP	115V	230V	460V	575V	2300V	230V	,460V	575V	2300V
½ ¾ 1	4 5.6 7.2	2 2.8 3.6	1 1.4 1.8	.8 1.1 1.4			*		
1½ 2 3	10.4 13.6	5.2 6.8 9.6	2.6 3.4 4.8	2.1 2.7 3.9		1	а 1		
5 7½ 10		15.2 22 28	7.6 11 14	6.1 9 11		2			
15 20 25		42 54 68	21 27 + 34	17 22 27	₹¥	53.	26	21	
30 40 50		80 104 130	40 52 65	32 41 52		63 83 104	32 41 52	26 33 42	
60 75 100		154 192 248	77 96 124	62 77 99	16 20 26	123 155 202	61 78 101	49 62 81	12 15 20
125 150 200		312 360 480	156 180 240	125 144 192	31 37 49	253 302 400	126 151 201	101 121 161	25 30 40

For full load currents of 208-volt and 220-volt motors, increase the corresponding 230-volt motor full-load current by 10 and 15 percent, respectively.

* These values of full-load current are for motors running at speeds usual for belted motors and motors with normal torque characteristics. Motors built for especially low speeds or high torques may require more running current, and multispeed motors will have full-load current varying with speed, in which case the nameplate current rating shall be used.

For 90 and 80 percent power factor the above figures shall be multiplied by 1.1 and 1.25 respectively. The voltages listed are rated motor voltages. The currents listed shall be permitted for system voltage ranges of 110 to 120, 220 to 240, 440 to 480, and 550 to 600 volts.

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ARTICLE 430 - MOTOR CIRCUITS, CONTROLLERS

Table 430-148. Full load Currents in AmperesSingle-Phase Alternating- Current Motors

The following values of full-load currents are for motors running at usual speeds and motors with normal torque characteristics. Motors built for especially low speeds or high torques may have higher full-load currents and multispeed motors will have full-load current varying with speed, in which case the nameplate current ratings shall be used. To obtain full load currents of 208-volt and 200-volt motors, increase corresponding 230-volt motor full-load currents by 10 and 15 percent, respectively. The voltages listed are rated motor voltages. The currents listed shall be permitted for

system voltage ranges of 110 to 120 and 220 to 240.

_	HP		115V	230V	
	1% 14 15 15 15 34		4.4 5.8 7.2 9.8 13.8	 2.2 2.9 3.6 4.9 6.9	
· · · · · · · · · · · · · · · · · · ·	1 1½ 2 3		16 20 24 34	8 10 12 17	
	5 7½ 10		3,56 80 100	 28 40 50	
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